

Acceptor-Induced Bulk Dielectric Loss in Superconducting Circuits on Silicon


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The performance of superconducting quantum circuits is primarily limited by dielectric loss due to interactions with two-level systems (TLSs). State-of-the-art circuits with engineered material interfaces are approaching a limit where dielectric loss from bulk substrates plays an important role. However, a microscopic understanding of dielectric loss in crystalline substrates is still lacking. In this work, we show that boron acceptors in silicon constitute a TLS bath that leads to an energy dissipation channel for superconducting circuits. We discuss how the electronic structure of boron acceptors leads to an effective TLS response in silicon. We sweep the boron concentration in silicon and demonstrate the bulk dielectric loss limit from boron acceptors. We show that boron-induced dielectric loss can be reduced in a magnetic field due to the spin-orbit structure of boron. This work provides the first detailed microscopic description of a TLS bath for superconducting circuits and demonstrates the need for ultrahigh-purity substrates for next-generation superconducting quantum processors.

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I. INTRODUCTION

Superconducting quantum processors are a leading platform for quantum computation [1,2] and simulation [3]. The performance of superconducting quantum processors is currently limited by high error rates [4] from coupling of qubits to unwanted energy dissipation channels such as quasiparticles, vortices, radiation, parasitic modes, and two-level systems (TLSs) [5,6]. TLSs are atomic-scale defects that are described by the standard tunneling model [7,8]. While the microscopic nature of TLSs remains elusive, they are primarily located inside amorphous materials at interfaces instead of the crystalline bulk substrate [9–11]. TLSs can have strong electric and elastic dipoles [12]. At the macroscopic level, this leads to dielectric loss, which is currently the dominant dissipation

mechanism for superconducting qubits [10,13]. Losses from interface TLSs can be reduced with improved surface treatments, material choices [14], and circuit designs with reduced surface participation [15]. With advances on these fronts, state-of-the-art superconducting qubits now show lifetimes approaching 1 ms [16]. For such low-loss devices, dielectric loss from the bulk substrate becomes non-negligible [17,18]. For instance, the best reported bulk loss tangent for sapphire (approximately 2×10^{-8}) limits the quality factor to 50 million [17] and the qubit lifetime to 1.5 ms. These results indicate the need for further advances in our understanding of bulk dielectric loss for substrates of superconducting circuits.

Silicon is a widely used material for quantum devices based on superconducting, spintronic, mechanical, and photonic systems [19–24]. High-resistivity ($>1000 \Omega \text{ cm}$), float-zone (FZ) -grown silicon substrates show bulk dielectric loss tangents below 5×10^{-7} [25–27] and are a standard choice to realize high-performance superconducting devices. However, a microscopic understanding of the origin of bulk dielectric loss in silicon is currently missing. In this work, we identify crystalline point defects associated with boron acceptors in silicon as a bulk TLS bath with strong electric dipolar coupling to superconducting circuits. We begin with a theoretical description of how the microscopic electronic structure of boron in silicon can result in TLS loss for superconducting microwave circuits. We use

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superconducting resonator loss measurements under varying doping concentration, microwave power, temperature, and device geometry to confirm the theoretical predictions. In addition, we experimentally show that the spin-orbit nature of boron acceptors results in a reduction of loss saturation power under a magnetic field. These observations are explained by the four-level fine structure of boron and support the identification of boron acceptors as the TLS bath. These results provide guidelines on silicon substrate purity requirements for low-loss qubits and constitute the first microscopic identification of a TLS bath in a crystalline substrate.

II. TWO-LEVEL SYSTEM AND ACCEPTOR HAMILTONIAN

For superconducting microwave circuits operating at low temperature and in the single-photon regime, defect-induced dielectric loss can arise from coupling to TLSs and bulk crystalline defects [Fig. 1(a)]. TLSs can be described by the standard tunneling model [Fig. 1(b)]. They strongly couple to electric (\mathbf{E}) and strain (\mathbf{S}) fields through the asymmetry energy of the double-well potential: $\varepsilon = \varepsilon_0 + 2\boldsymbol{\gamma} \cdot \mathbf{S} + 2\mathbf{p} \cdot \mathbf{E}$. Typical TLS has a deformation potential ($\boldsymbol{\gamma}$) of 1 eV [28] and an electric dipole moment (\mathbf{p})

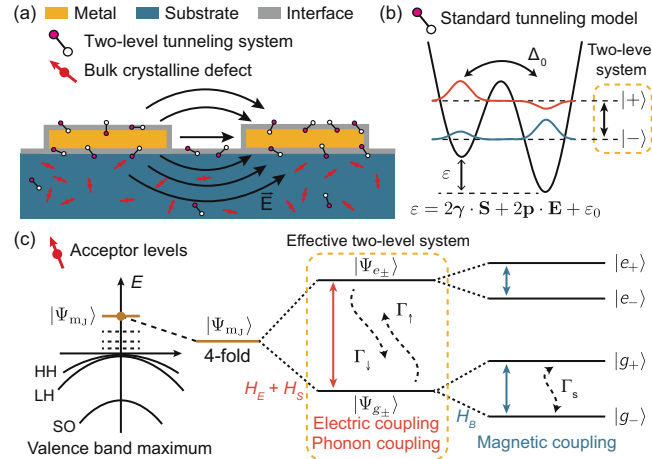


FIG. 1. Comparison of amorphous two-level systems and boron acceptors in silicon. (a) Schematic of the cross section of planar superconducting devices. TLS loss originates from defects or disorder in the amorphous interface layers and the bulk dielectric substrate. Bulk crystalline defects may also contribute to TLS loss. (b) Standard tunneling model of TLS. The asymmetry energy (ε) of the double-well potential couples strongly to electric field (\mathbf{E}) and strain (\mathbf{S}) through electric dipole (\mathbf{p}) and deformation potential ($\boldsymbol{\gamma}$). Δ_0 denotes the tunneling energy between the two wells. (c) Left: valence band maximum of silicon showing the split-off (SO), heavy-hole (HH), and light-hole (LH) bands. Right: electronic structure of boron acceptors in the hole picture showing coupling to electric, strain, and magnetic fields as described by the interaction Hamiltonians H_E , H_S , and H_B , respectively, in the main text. Γ_\uparrow (Γ_\downarrow), orbital relaxation rate. Γ_s , relaxation rate between the generalized spin states.

of 3 D [29]. The TLS can be described by the following Hamiltonian [30]:

$$H = \frac{1}{2} \Delta E \sigma_z + (\boldsymbol{\gamma} \cdot \mathbf{S} + \mathbf{p} \cdot \mathbf{E}) \left(\frac{\varepsilon_0}{\Delta E} \sigma_z + \frac{\Delta_0}{\Delta E} \sigma_x \right), \quad (1)$$

where $-\Delta_0$ ($\Delta_0 > 0$) is the tunneling matrix element between the two potential wells, ε_0 is the static asymmetry energy, $\Delta E = \sqrt{\varepsilon_0^2 + \Delta_0^2}$ is the energy splitting between the two levels, and σ denotes the Pauli operator. Because of their amorphous nature, TLS parameters are sampled from a broad distribution.

In contrast to highly disordered TLS defects in amorphous materials, silicon hosts high-quality spin (spin-orbit) qubits based on crystalline donor (acceptor) defects [31–33]. The electronic structures of donors and acceptors are well studied and can be used to predict their impact on superconducting circuits. Donor (e.g., phosphorus or bismuth) defects weakly couple to their environment via magnetic dipole interactions and show long spin lifetimes [31,32,34]. Magnetic dipole interactions are much weaker compared to electric dipole interactions, and the donor spin resonances are typically detuned from circuits at zero magnetic field. Donor defects, therefore, cannot result in the frequently observed saturable TLS loss in superconducting circuits. In contrast, other bulk crystalline defects can display Hamiltonians similar to TLSs and cause dielectric loss. In particular, acceptor (e.g., boron or aluminum) defects have strong electric and elastic dipoles and, therefore, exhibit short lifetimes [35–37]. In this work, we investigate acceptors as a potential origin of a bulk TLS bath in silicon. Our study focuses on boron defects, one of the most common acceptor-type contaminants in silicon.

The electronic structure of boron acceptors inherits the properties of the valence band maximum of silicon [Fig. 1(c)]. The ground state is an effective spin-3/2 system with a twofold orbital degeneracy and a twofold spin degeneracy. The linear coupling of the ground state to magnetic (H_B), electric (H_E), and strain (H_S) fields can be described as [38]

$$H_B = \mu_B [g_1 (J_x B_x + \text{c.p.}) + g_2 (J_x^3 B_x + \text{c.p.})], \quad (2)$$

$$H_E = \frac{p_B}{\sqrt{3}} (E_x \{J_y, J_z\}_+ + \text{c.p.}), \quad (3)$$

$$H_S = \gamma_B S_{xx} J_x^2 + \frac{\gamma'_B}{\sqrt{3}} S_{xy} \{J_x, J_y\}_+ + \text{c.p.}, \quad (4)$$

where J is the spin-3/2 operator, $\{\cdot, \cdot\}_+$ denotes the anti-commutator, c.p. denotes cyclic permutation, $g_1 = -1.07$ and $g_2 = -0.03$ are the g factors [36], $p_B = 0.26$ D is the electric dipole moment [36], and $\gamma_B = -1.42$ eV and $\gamma'_B = -3.7$ eV are deformation potentials [37]. The twofold orbital degeneracy can be lifted with static lattice strain and/or electric field ($H_S + H_E$), which results in a TLS-like level structure. Within each orbital branch, the spin degeneracy

can be lifted with a static magnetic field (H_B). The magnitudes of the electric dipole (p_B) and deformation potentials (γ_B, γ'_B) for boron acceptors are similar to those of conventional TLSs [\mathbf{p} and γ in Eq. (1)] in amorphous materials. The strong correspondence in orbital structures and dipole strengths between borons and TLSs suggests that boron acceptors should lead to saturable dielectric loss like conventional TLSs.

III. PROBING BORON-INDUCED DIELECTRIC LOSS

In the following, we test the hypothesis of boron acceptors constituting a bulk TLS bath and a strong dielectric loss channel. We use superconducting niobium resonators to probe acceptor-induced loss under varying acceptor concentration, temperature, power, and magnetic fields. To access a bulk dielectric loss-dominated regime, we first study the geometric dependence of loss under our fabrication procedure with quarter-wave resonators of varying dimensions [Fig. 2(a)] and frequencies ranging from 4.3 to 7.7 GHz. For resonators on both undoped ($[B] < 8 \times 10^{11} \text{ cm}^{-3}$) and boron-doped ($[B] = 7.4 \times 10^{14} \text{ cm}^{-3}$) FZ silicon, we observe improvement of internal quality factors (Q_i) at high excitation powers (see Fig. 6). The power dependence shows the presence of TLS loss in both substrates. For undoped silicon, the single-photon Q_i scales inversely with the surface participation ratio, indicating the loss is dominated by surface TLSs [Fig. 2(b)] [10]. On boron-doped silicon, the single-photon Q_i does not show such an inverse scaling with surface participation [Fig. 2(b)]. The energy participation in the bulk silicon substrate is about 90% due to the high dielectric constant of silicon and depends weakly on resonator geometry (see Table II). The absence of a negative correlation between the surface participation ratio and Q_i confirms that TLS loss is no longer surface limited on boron-doped silicon and that we are probing TLSs in the bulk silicon substrate [18]. We note that there is a weak positive correlation between the surface participation ratio and Q_i on boron-doped silicon. Such correlations cannot be explained by a constant bulk loss tangent and may be related to a geometry-dependent TLS spectrum due to interface strain (see Appendix C 4).

We use the resonator design with the lowest surface participation to probe TLS loss in boron-doped silicon ($[B] = 7.4 \times 10^{14} \text{ cm}^{-3}$). With this design and boron concentration, the surface-limited single-photon Q_i is about 2 orders of magnitude higher than the bulk-limited single-photon Q_i , and the loss behavior will be dominated by TLSs in the bulk. The sample contains eight quarter-wave resonators evenly spaced in a 1 GHz band centered around 6 GHz [see Fig. 5(b)]. The average power-dependent Q_i of the resonators at different mixing chamber temperatures (T_{MJC}) is plotted in Fig. 2(c). For all resonators, Q_i consistently shows strong reduction at low powers. At the same time, low-power Q_i increases when thermal energy is comparable

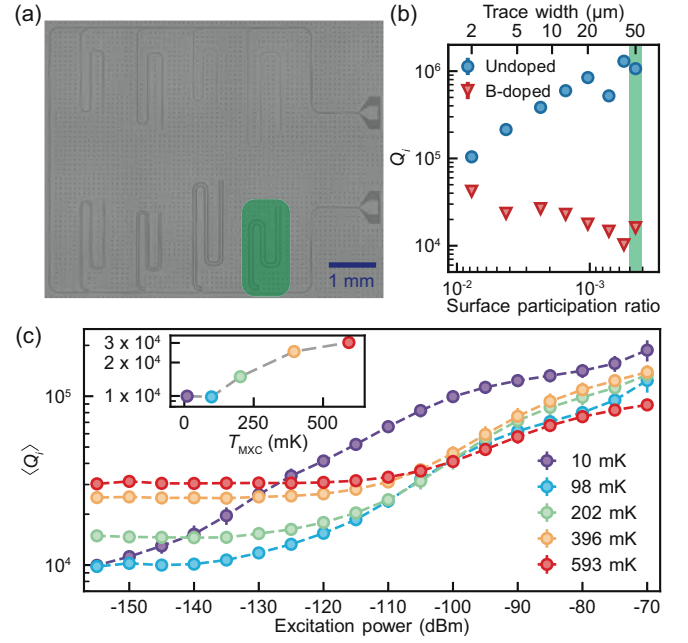


FIG. 2. Bulk two-level system loss in a boron-doped silicon substrate. (a) Optical image of the device with eight quarter-wave resonators capacitively coupled to a shared feedline. The resonator trace width is swept from 2 to 50 μm to access different surface participation ratios while maintaining 50 Ω impedance. The highlighted resonator (green) has the lowest surface participation. (b) Internal quality factor (Q_i) at single-photon level as a function of surface participation ratio including contributions from metal-vacuum, metal-substrate, and substrate-vacuum interfaces. Q_i of resonators on undoped (doped, $[B] = 7.4 \times 10^{14} \text{ cm}^{-3}$) silicon is measured at $\langle n \rangle \approx 0.1$ ($\langle n \rangle \approx 0.01$). Data points shaded in green are measured from the lowest surface participation ratio resonator highlighted in (a). (c) Power-dependent Q_i at different temperatures for low surface participation ratio resonators on boron-doped silicon. $\langle Q_i \rangle$ represents the average of power dependence from eight resonators. Inset: temperature dependence of low-power Q_i (excitation power -155 dBm , $\langle n \rangle < 0.1$).

to the resonator frequency [Fig. 2(c), inset]. This thermal saturation feature is another indication that bulk loss tangent in boron-doped silicon is dominated by TLS-like atomic defects [5]. Since boron concentration is the main difference between the doped and undoped substrates, observing TLS-like power and thermal saturation of the bulk-limited loss confirms the TLS-acceptor correspondence discussed in Fig. 1. We, therefore, conclude that boron acceptors act as a TLS loss channel in the bulk substrate. We note that the bulk TLS loss from boron defects appears broadband ($> 1 \text{ GHz}$) based on the consistent saturation behaviors of resonators at different frequencies. This broadband behavior is likely related to a broad inhomogeneous distribution of boron orbital splittings due to an inhomogeneous strain distribution near the metal-silicon interface (see Figs. 12 and 13 [39]) and the local disorder in the environment of individual defects. The uncontrolled strain distribution poses significant challenges in observing well-defined

TABLE I. Specifications of silicon wafers.

Wafer type	Vendor	Resistivity (Ω cm)	Growth method	Boron concentration (cm^{-3})
Undoped	NOVA Electronic Materials	>10000	Float zone	$<8 \times 10^{11}$
Phosphorus doped	University Wafer	50–70	Float zone	$<8 \times 10^{11}$
Boron doped no. 1	University Wafer	>2500	Float zone	4.6×10^{12}
Boron doped no. 2	University Wafer	>50	Float zone	6.7×10^{13}
Boron doped no. 3	University Wafer	8–13	Float zone	7.4×10^{14}
Boron doped no. 4	WaferPro	1–10	Czochralski	2.5×10^{15}

transitions from boron ensembles [33]. At the same time, performing direct loss tangent measurement on low- or high-strain samples may reveal a different loss behavior [17,40].

We quantify the impact of acceptor-induced dielectric loss on superconducting qubits by studying superconducting resonator low-power Q_i as a function of dopant type and doping concentration. Our first-principles estimation (see Appendix C 3) suggests acceptor-induced dielectric loss can be significant due to the high (approximately 90%) energy participation of the bulk. However, the exact magnitude of acceptor-induced loss tangent strongly depends on the strain distribution and the electric dipole moment and necessitates experimental characterization.

We fabricate resonators identical to the ones studied in Fig. 2(c) on undoped, phosphorus-doped, and boron-doped substrates (see Table I). The average low-power Q_i at $T_{\text{MXC}} = 8$ mK as a function of doping concentration is summarized in Fig. 3. For undoped silicon and lightly boron-doped ($[B] = 4.5 \times 10^{12} \text{ cm}^{-3}$) silicon, low-power Q_i saturates around 10^6 , consistent with the surface TLS limit in Fig. 2(b). For substrates with higher boron concentration, Q_i shows strong anticorrelation with boron concentration. This anticorrelation is consistent with the assignment of boron acceptors as a bulk TLS bath. We extrapolate the bulk limit of Q_i from boron doping for state-of-the-art devices using a linear fit of loss and boron doping. The extrapolation suggests bulk-limited Q_i would be limited to 10^7 and 10^8 for boron concentrations of 10^{12} and 10^{11} cm^{-3} , respectively. We note that state-of-the-art quantum devices have lifetimes (T_1) around 1 ms, corresponding to a quality factor of $Q = 2\pi f \times T_1 \approx 3 \times 10^7$ at $f = 5$ GHz. Based on our extrapolation and considering bulk dielectric loss alone, realizing such high-performance devices on silicon requires the use of ultrahigh-purity silicon with boron concentration below $3 \times 10^{11} \text{ cm}^{-3}$ (resistivity $>50 \times 10^3 \Omega$ cm). Further lifetime improvement will necessitate high-purity substrates free of boron defects and may require advancements in silicon wafer growth. We note that low-power Q_i of resonators on phosphorus-doped silicon does not show excess loss from the bulk. The lack of phosphorus-induced loss is consistent with the prediction based on its electronic structure, which does not contain any orbital degeneracy in its ground state (see Fig. 11 [41]).

IV. MAGNETIC FIELD RESPONSE OF BORON-INDUCED DIELECTRIC LOSS

Having shown the bulk TLS behavior of boron acceptors, we turn to probing key distinctions between boron and conventional TLS [12]. In the following, we demonstrate that the spin-orbit coupling and four-level nature of boron acceptors lead to a strong magnetic field dependence of boron-induced dielectric loss. Figure 4(a) shows the level structure of boron acceptors. Under zero magnetic field, the level structure resembles the structure of a conventional

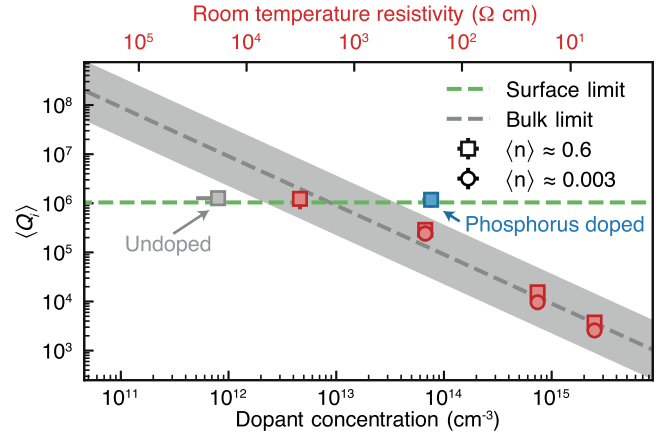


FIG. 3. Dielectric loss in silicon under different doping conditions. For substrates with high boron concentration, we show the average Q_i with $\langle n \rangle \approx 0.003$ (red circle) and $\langle n \rangle \approx 0.6$ (red square). For substrates with low boron concentration, Q_i is surface TLS limited, and we report the average Q_i with $\langle n \rangle \approx 0.6$ due to the challenge of Q_i extraction with an overcoupled ($Q_e \approx 4 \times 10^4$) resonator design (see Fig. 7). Q_i on phosphorus-doped silicon is consistent with the surface TLS limit. The gray dashed line is a linear fit [$\log Q_i = -\log(a \times \rho)$] of loss at $\langle n \rangle \approx 0.003$ to boron concentration (ρ) and is extrapolated to a boron concentration of $5 \times 10^{10} \text{ cm}^{-3}$. The gray band represents the 95% confidence band. The boron concentration is measured using secondary ion mass spectrometry (SIMS), while phosphorus concentration is estimated using wafer resistivity. The boron concentration in undoped silicon is below the detection limit of SIMS ($8 \times 10^{11} \text{ cm}^{-3}$). The boron-doped silicon with highest doping concentration is Czochralski grown, whereas all other substrates are FZ grown. The top x axis shows the expected room-temperature wafer resistivity from boron doping.

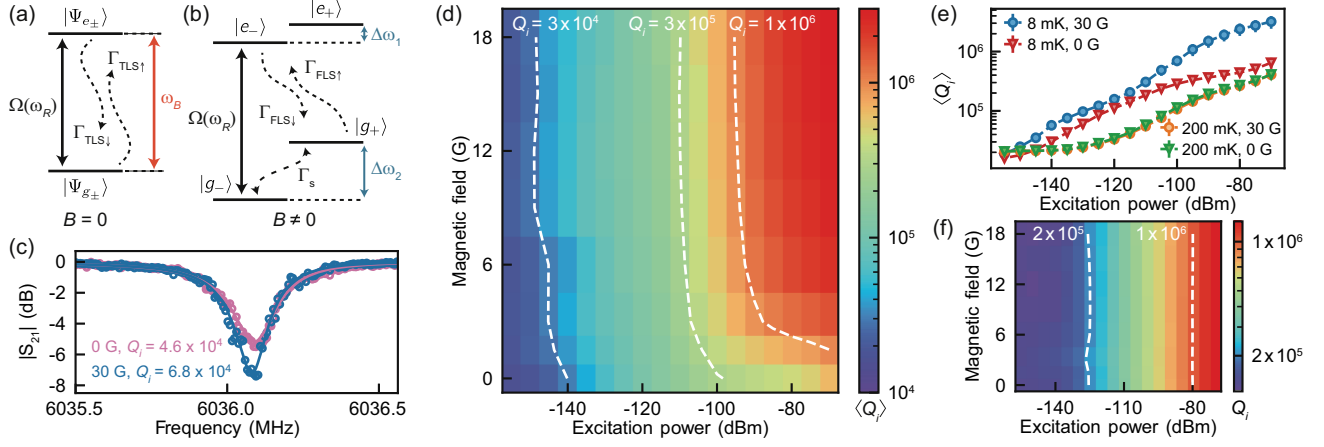


FIG. 4. Magnetic response of four-level system dielectric loss in boron-doped silicon. Simplified level structure of boron acceptors under (a) zero and (b) a small magnetic field. (a) $\Gamma_{\text{TLS}\uparrow}$ ($\Gamma_{\text{TLS}\downarrow}$), orbital relaxation rate; ω_B , boron resonance frequency. (b) The effective two-level structure of boron is modified to a four-level system in a magnetic field. $\Gamma_{\text{FLS}\uparrow}$ ($\Gamma_{\text{FLS}\downarrow}$), orbital relaxation rate between $|e_-\rangle$ and $|g_+\rangle$; orbital decay paths between other states are not shown for simplicity. Γ_s , relaxation rate between the generalized spin states $|g_+\rangle$ and $|g_-\rangle$. $\Omega(\omega_R)$, Rabi frequency at the resonator frequency (ω_R). (c) Low-power (-135 dBm) $|S_{21}|$ measurement of a resonator on boron-doped silicon at $T_{\text{MXC}} = 8$ mK. Q_i increases in a small magnetic field (30 G). (d) Power-dependent Q_i under different magnetic fields for resonators on boron-doped silicon. The dashed lines are interpolated Q_i isocontours. Q_i shows an overall increase at higher magnetic fields. (e) Power-dependent Q_i measured at $T_{\text{MXC}} = 8$ and 200 mK under zero magnetic field and 30 G. (f) Power-dependent Q_i under different magnetic fields for a resonator with $2 \mu\text{m}$ trace on undoped silicon. No magnetic field response is observable. Data in (d) and (e) represent the average Q_i of eight resonators.

TLS, with stray strain and electric field determining the orbital splitting (ω_B). Magnetic fields lift spin degeneracies and result in a four-level structure [Fig. 4(b)]. The effective g factors within the two orbital branches are determined by the exact strain environment, which, in general, leads to unequal Zeeman splittings ($\Delta\omega_1 \neq \Delta\omega_2$). When the orbital splitting is much greater than spin splitting, the lower orbital branch exhibits two long-lived generalized spin states [33].

We fabricate resonators with narrow traces ($10 \mu\text{m}$) and wide gaps ($40 \mu\text{m}$) on boron-doped silicon ($[\text{B}] = 7.4 \times 10^{14} \text{ cm}^{-3}$) to study how the loss is modified under an in-plane magnetic field due to the four-level structure of boron. The narrow-trace geometry is chosen to mitigate vortex formation [42], while the wide-gap configuration helps maintain a low surface-participation ratio for detecting bulk loss. Under a small magnetic field (30 G), we observe an improvement in the low-power Q_i compared to the zero-field case [Fig. 4(c)]. We further investigate how loss evolves under a magnetic field by measuring the power-dependent Q_i as a function of magnetic field [Fig. 4(d)]. We observe three key features: (i) The saturation power of boron-induced loss is reduced by an order of magnitude under a nonzero magnetic field [Figs. 4(e) and 16], (ii) the loss reduction induced by magnetic field saturates at a magnetic field as low as 5 G, and (iii) high-power Q_i shows a drastic improvement under a magnetic field.

A simplified description of the change in saturation power in a magnetic field can be explained using the four-level system dynamics of boron acceptors in a magnetic

field. Under zero magnetic field, boron acceptors are equivalent to standard TLSs. Driving the resonator at ω_R excites the nearby boron defects ($\omega_B \approx \omega_R$) with a rate Ω . Acceptor-induced dielectric loss is saturated when the excitation rate is comparable to the fast orbital relaxation rate $\Omega \sim \Gamma_{\text{TLS}\downarrow}/2$. For magnetic fields where the differential Zeeman splitting $|\Delta\omega_2 - \Delta\omega_1|$ becomes greater than the resonator and boron linewidths (approximately 5 G), transition associated with one of the ground states ($|g_-\rangle$) is selectively driven. Therefore, the ground state population is pumped to the other long-lived dark state ($|g_+\rangle$) with a rate of approximately $4|\Omega|^2/\Gamma_{\text{FLS}\downarrow}$. Such microwave-pumped boron acceptors are trapped in $|g_+\rangle$ and decoupled from the resonator. This decrease of the effective number of TLSs results in reduced dielectric loss. In addition, the loss saturation occurs at a lower power where the pumping rate equals the dark state decay rate ($4|\Omega|^2/\Gamma_{\text{FLS}\downarrow} \sim \Gamma_{\text{FLS}\uparrow}$), assuming $\Gamma_s \ll \Gamma_{\text{FLS}\downarrow, \uparrow}$. We use the measured ratio of saturation powers with and without magnetic fields to estimate the thermal occupancy (\bar{n}) and the effective sample temperature. Our master equation model for four-level system saturation indicates an effective sample temperature of approximately 75 mK based on the measured saturation power ratios (see Fig. 16 for a detailed analysis). The inferred effective temperature here is comparable to the effective temperatures reported in other studies [43–46]. At elevated temperatures, the magnetic response becomes weaker (see Fig. 9) due to exponential activation of thermal occupancy and $\Gamma_{\text{FLS}\uparrow}/\Gamma_{\text{FLS}\downarrow} = \bar{n}/(1 + \bar{n})$, where $\bar{n} < 1$. We observe a complete disappearance of dielectric loss

reduction in response to magnetic field at $T_{\text{MXC}} = 200$ mK [Fig. 4(e)]. Finally, we note that the loss reduction is higher at higher excitation powers, which may be accounted by the reduction of loss from a large ensemble of off-resonant boron acceptors.

We also perform a magnetic field study of the saturation behavior of conventional TLSs at surfaces. Prior magnetic field studies mostly focused on using electron spin resonance (ESR) to study the spin degree of freedom of surface TLSs [47–50]. However, ESR probes the weak magnetic resonances, leaving the electric dipole resonances largely unexplored. To our knowledge, magnetic response of the saturation behavior of amorphous TLSs has not been reported before. We perform our study on various resonators fabricated on undoped silicon. These resonators show loss contribution from amorphous TLSs either due to their large surface participation ratios or due to a high density of intentionally introduced amorphous TLSs by drop casting hydrogen silsesquioxane (HSQ, a spin-on-glass). In contrast to the acceptor-induced loss, the saturation behavior of amorphous TLS-induced loss remains unchanged in small magnetic fields [Figs. 4(f) and 10]. We emphasize that the lack of magnetic field response in our experimental regime cannot rule out the existence of magnetic dipole moments in amorphous TLSs. Instead, the observation indicates that surface TLSs do not have a differential Zeeman splitting in different orbital states [Fig. 4(b)].

V. CONCLUSION

In conclusion, we report the first microscopic identification of a TLS bath from bulk crystalline defects in silicon. Our study indicates that the acceptor-induced loss can act as a near-future limiting factor for state-of-the-art superconducting quantum devices on silicon. We show that the acceptor-induced dielectric loss can be reduced under a small magnetic field. These results also show the need for ultrahigh-purity silicon wafers to enable next-generation superconducting qubits. We note that our observations apply to other acceptors in silicon which display similar electronic structures [51,52]. Accurately estimating dielectric loss from first principles will require precise measurements of the acceptor dipole moment and inhomogeneous distribution. In our model, strain plays a critical role in determining the acceptor inhomogeneous distribution. Future experiments to verify the strain-induced inhomogeneous distribution should focus on measuring the dielectric loss at higher frequencies and studying dielectric loss with tunable strain. In parallel to improvements to substrate purity, the acceptor-induced dielectric loss may be mitigated through charge engineering of the acceptors using compensation doping or field ionization and spectral engineering by tuning the acceptor density of states with electric and strain fields [29,53]. Further loss suppression can be achieved using vacuum-gap capacitors [54] or

engineering the acceptor dynamics with phononic crystals [55,56]. Finally, further engineering of interactions with boron acceptors can enable their use as spin-orbit qubits strongly coupled to microwave and mechanical resonators [33,57–62].

The designs for different chips used in our study are openly available [63].

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APPENDIX A: SUPPLEMENTARY EXPERIMENTAL METHODS

1. Experimental setup

The devices were measured using a vector network analyzer (Copper Mountain C1209) in a dilution refrigerator (Bluefors, BF-LD250) with a base temperature of approximately 8 mK at the mixing chamber. The output level of the network analyzer was sometimes attenuated (Vaunix LDA-908V or Mini-Circuits fixed attenuators) or amplified (Mini-Circuits ZX60-83LN-S+) to increase the dynamic range of the excitation power. The microwave excitation on the input line of the dilution refrigerator was attenuated at different stages (20 dB at 4 K, 20 dB at 100 mK, 20 dB at mixing chamber) using cryogenic attenuators (XMA Corporation, 2082-6418-20-CRYO Bulk) with a total attenuation of 60 dB. After attenuation, the excitation was filtered using an Eccosorb IR filter (Bluefors). We connected the input line and the output line to a pair of rf switches (Radiall R583423141) for asynchronous device multiplexing. For microwave detection, the signal was isolated with two isolators (Low Noise Factory LNF-CIC4_8A) and filtered with a bandpass filter (Keenlion KBF-4/8-2S). After isolation and filtering, the signal was amplified with a HEMT amplifier (Low Noise

Factory LNF-LNC4_8C) at 4 K followed by a low noise amplifier at room temperature (Mini-Circuits ZX60-123LN-S+).

The devices were packaged in a copper box and mounted vertically inside two cylindrical magnetic shields (Cryo-NETIC) for most measurements. For magnetic field dependence measurements, the devices were mounted outside the magnetic shields. A superconducting coil (field factor approximately 300 G/A for the experimental sample-coil distance) made from NbTi wires (Supercon SC-54S43-0.152 mm) was mounted below the device to provide an in-plane magnetic field.

2. Device fabrication

Prior to metallization, we cleaned the 6'' silicon wafers in piranha solution (5 min) and dilute (25:1) HF. The cleaned wafers were loaded into a dc sputtering system (MRC 943). The wafers were *in situ* sputter-etch cleaned and sputtered with approximately 200 nm of niobium. Coplanar-waveguide resonators were patterned with optical lithography using a maskless aligner (Heidelberg MLA150) and subsequently dry etched (Lam Research) with Cl_2 chemistry, followed by deionized water passivation and photoresist stripping (1165 Remover). The wafers were then diced (Disco DAD3240) into $1\text{ cm} \times 1\text{ cm}$ chips with a protective photoresist layer. Upon photoresist stripping, the chips were dipped in buffered oxide etch (5:1) for approximately 35 min, wire bonded onto a printed circuit board (PCB), packaged in a copper box, and cooled down in a dilution refrigerator with a base temperature of 8 mK.

3. Silicon substrate for bulk loss characterization

To study the excess dielectric loss induced from bulk crystalline defects, we fabricated superconducting resonators following procedures in Appendix A 2 on prime-grade silicon wafers with different doping conditions. Each wafer was specified with a wafer resistivity. Secondary ion mass spectrometry (EAG Eurofins) was used to accurately

determine the boron concentration in each wafer (detection limit $[\text{B}] = 8 \times 10^{11}\text{ cm}^{-3}$). The specifications of different wafers are summarized in Table I.

4. Resonator design

Coplanar-waveguide resonators of different geometries were fabricated for different studies throughout the work. The optical images of samples with different resonator designs are shown in Fig. 5.

Surface loss study.—For the loss study with different surface participation, we swept the trace and gap widths of quarter-wave resonators by more than an order of magnitude while maintaining a $50\ \Omega$ impedance [Fig. 5(a)]. The resonators were designed to have a coupling quality factor of approximately 300×10^3 . Their lengths were swept for frequency multiplexing from 4 to 7.5 GHz. We estimated the total surface participation ratio for each resonator geometry using the analytical formalism developed in Ref. [64], assuming a 3 nm surface contamination layer with a dielectric constant of 10. Similar analytical formalism has been developed in Ref. [15]. The surface participation ratio includes contributions from metal-vacuum, metal-substrate, and substrate-vacuum interfaces. We also calculated the energy participation ratio in bulk silicon using electrostatic simulation with COMSOL MULTIPHYSICS. The parameters of the resonators are summarized in Table II. The resonators with high surface participation ratio (trace widths 2, 4, and $8\ \mu\text{m}$) are also used for magnetic field study.

Bulk loss study.—To characterize the bulk dielectric loss, we fabricated quarter-wave resonators with a trace width of $50\ \mu\text{m}$ and a gap width of $33.75\ \mu\text{m}$ [Fig. 5(b)]. Each chip contains eight resonators, and the resonator lengths were swept for frequency multiplexing in a 1 GHz band centered around 6 GHz. The coupling quality factor was reduced to around 40×10^3 to improve the sensitivity to detect low- Q resonances on boron-doped substrates.

Magnetic field study (bulk loss).—To probe the magnetic field response of loss on boron-doped substrates, we

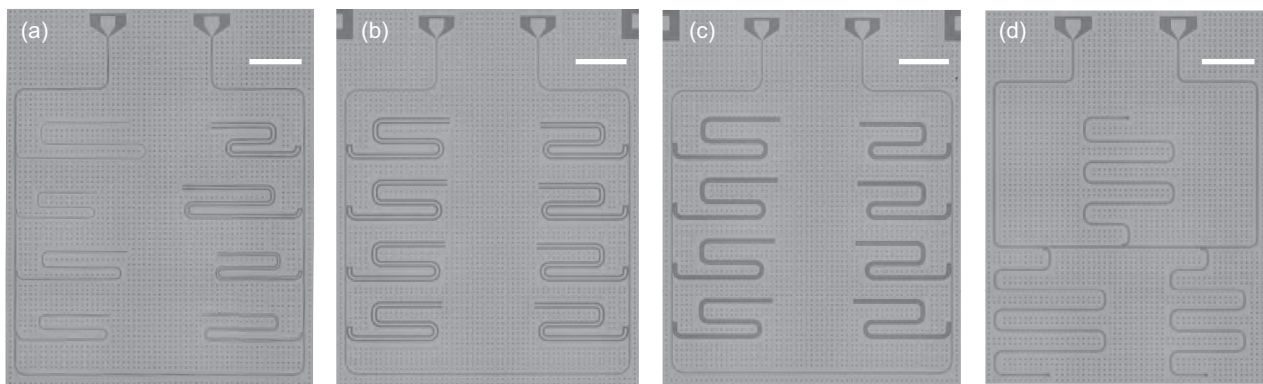


FIG. 5. Optical images of samples with different resonator designs. (a) Resonator design with different surface participation ratio. (b) Resonator design with low surface participation ratio. (c) Resonator design with narrow trace and wide gap for magnetic field study. (d) Resonator design for magnetic field study of surface loss. The scale bar represents 1 mm.

TABLE II. Resonator parameters for geometric sweeping.

Resonator no.	Trace width (μm)	Gap width (μm)	Surface participation ratio	Bulk participation ratio
1	2	1.42	7.75×10^{-3}	9.04×10^{-1}
2	4	2.78	4.27×10^{-3}	9.12×10^{-1}
3	8	5.4	2.35×10^{-3}	9.16×10^{-1}
4	13	8.8	1.52×10^{-3}	9.18×10^{-1}
5	20	13.5	1.03×10^{-3}	9.19×10^{-1}
6	30	20.25	7.2×10^{-4}	9.20×10^{-1}
7	40	27	5.5×10^{-4}	9.20×10^{-1}
8	50	33.75	4.5×10^{-4}	9.20×10^{-1}

fabricated quarter-wave resonators with a trace width of $10 \mu\text{m}$ and a gap width of $40 \mu\text{m}$ [Fig. 5(c)]. Such dimensions were chosen to mitigate vortex losses due to magnetic field while maintaining a relatively low surface participation. Each chip contains eight resonators, and the resonator lengths were swept for frequency multiplexing in a 1 GHz band centered around 6 GHz. The coupling quality factor was designed to be around 50×10^3 .

Magnetic field study (surface loss).—To probe the magnetic field response of loss induced by surface TLSs on an undoped substrate, we fabricated half-wave resonators with a trace width of $16.3 \mu\text{m}$ and a gap width of $10 \mu\text{m}$ [Fig. 5(d)]. After fabrication and the initial round of measurements, we intentionally introduce excessive amorphous TLS on the surface by drop casting HSQ. The chip contains three resonators with frequencies at 4.8, 5.7, and 6.6 GHz. The coupling quality factor was designed to be around 300×10^3 .

The different chip designs together with the measurements performed on each of them are summarized in Table III.

5. Resonator measurement and data analysis

We probe the resonator loss by measuring the transmission through the microwave feedline on each chip. With the side-coupled configuration, the resonance of each resonator shows up as a narrow dip in $|S_{21}|$. With the large variation of resonator loss on different substrates, the measurement bandwidth for each resonator were adjusted with a total number of 500–1000 sampling points using an

IF bandwidth of 10 Hz. S_{21} traces were averaged for noise reduction for low power measurements.

The complex S_{21} traces were fitted using

$$S_{21}(f) = a \times e^{i[\phi + 2\pi(f - f_{\text{start}})\tau]} \frac{1 - Q/Q_c \times (1 + 2idf/f_0)}{1 + 2iQ(f - f_0)/f_0}, \quad (\text{A1})$$

where a represents the baseline transmission away from the resonance, ϕ represents the phase offset, f_{start} is the starting frequency of the measurement, τ represents the group delay, Q represents the total quality factor, Q_c represents the coupling quality factor, f_0 is the center frequency of the resonator, and df is the asymmetric factor to account for impedance mismatch.

The average photon number ($\langle n \rangle$) inside the resonator with input power P_{in} can be estimated from the input-output theory [65]. Here, we describe the formalism for a generic coupling scheme where a cavity couples to two waveguide ports. The dynamics of the cavity field \hat{a} is

$$\frac{d\hat{a}}{dt} = -i(\omega_0 - \omega)\hat{a} - \frac{\kappa_i + \kappa_{e1} + \kappa_{e2}}{2}\hat{a} + \sqrt{\kappa_{e1}}s_{1+} + \sqrt{\kappa_{e2}}s_{2+}, \quad (\text{A2})$$

where ω_0 (ω) denotes the cavity (drive) frequency, κ_{e1} and κ_{e2} denote the coupling rate from the cavity to the two waveguide ports, s_{1+} (s_{2+}) denotes the input field from waveguide port 1 (port 2), and κ_i denotes the intrinsic decay rate of the cavity, respectively. In the steady state ($d\hat{a}/dt = 0$), the cavity field is

$$\hat{a} = \frac{\sqrt{\kappa_{e1}}s_{1+} + \sqrt{\kappa_{e2}}s_{2+}}{i(\omega_0 - \omega) + (\kappa_i + \kappa_{e1} + \kappa_{e2})/2}. \quad (\text{A3})$$

For our resonators with a side-coupled configuration and single-sided excitation, we have $\kappa_{e1} = \kappa_{e2} = \kappa_e/2$ and $s_{2+} = 0$. On resonance ($\omega_0 = \omega$), the steady state cavity field is

$$\langle \hat{a} \rangle = \frac{\sqrt{\kappa_e/2}s_{1+}}{(\kappa_i + \kappa_e)/2}, \quad (\text{A4})$$

and we can convert input power ($P_{\text{in}} = \hbar\omega_0|s_{1+}|^2$) to average photon number ($\langle n \rangle$) following Ref. [66]:

TABLE III. Summary of parameters and measurements for different resonator designs.

Chip design	Trace (μm)	Gap (μm)	Surface participation ratio	Figures
Surface loss study	2–50	1.42–33.75	7.75×10^{-3} – 4.5×10^{-4}	2(b), 4(f), 6, 10(a), 10(b)
Bulk loss study	50	33.75	4.5×10^{-4}	2(c), 3, 7
Magnetic field study (bulk loss)	10	40	9.8×10^{-4}	4(c)–4(e), 8, 9, 16
Magnetic field study (surface loss)	16.3	10	1.3×10^{-3}	10(c), 10(d)

$$\langle n \rangle = |\langle \hat{a} \rangle|^2 = \frac{2\kappa_e}{(\kappa_e + \kappa_i)^2} \frac{P_{\text{in}}}{\hbar\omega_0} = \frac{2}{\hbar\omega_0^2} \frac{Q^2}{Q_e} P_{\text{in}}, \quad (\text{A5})$$

where Q (Q_e) denotes the loaded (coupling) quality factor and P_{in} is the input power at the resonator. By measuring the loss through a closed loop of cables when the dilution

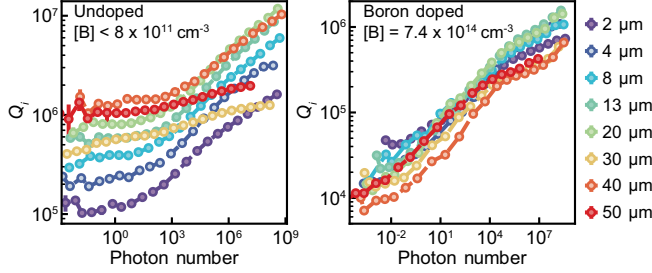


FIG. 6. Power-dependent measurement on individual resonators on undoped silicon (left) and boron-doped silicon (right) with varying surface participation. The legend denotes the signal trace width for each resonator.

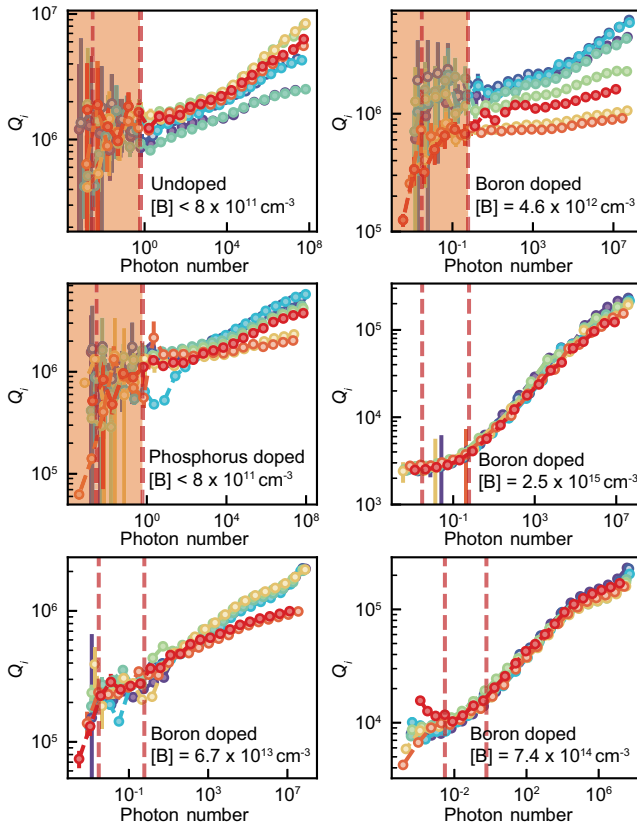


FIG. 7. Power dependence of Q_i for individual resonators on different silicon substrates. For devices with low loss, accurately extracting high Q_i at low powers is challenging due to the extremely overcoupled resonator design ($Q_e \ll Q_i$). The orange shaded regions indicate such low-power regions with fitting results dominated by noise. The dashed vertical lines indicate $\langle n \rangle \approx 0.003$ and $\langle n \rangle \approx 0.6$, respectively.

fridge is at its base temperature, we estimated a total attenuation of 85 dB in the input microwave chain due to cryogenic attenuators, as well as attenuation from coaxial cables, and insertion loss from filters, rf switch, and PCB.

APPENDIX B: SUPPLEMENTARY DATA AND MEASUREMENTS

1. Surface participation dependence of Q_i

In Fig. 2(b), we presented the low-power Q_i of resonators with different surface participation. The power-dependent Q_i measurements on each resonator are shown in Fig. 6.

2. Doping dependence of Q_i

In Fig. 3, we presented the average low-power Q_i of resonators fabricated on different silicon substrates. The power-dependent Q_i measurements on each resonator are shown in Fig. 7.

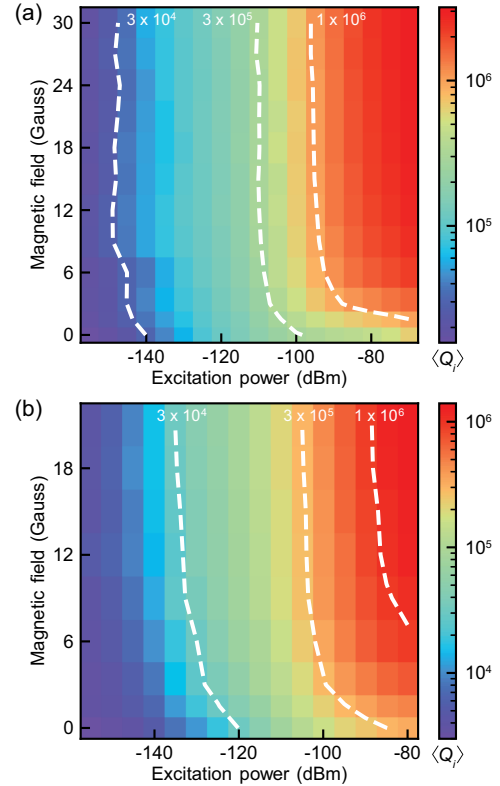


FIG. 8. Magnetic field dependence of Q_i on resonators fabricated on (a) a float-zone-grown substrate with $[B] = 7.4 \times 10^{14} \text{ cm}^{-3}$ and (b) a Czochralski-grown substrate with $[B] = 2.5 \times 10^{15} \text{ cm}^{-3}$. The dashed lines are interpolated contour lines for $Q_i = 3 \times 10^4$, $Q_i = 3 \times 10^5$, and $Q_i = 1 \times 10^6$ as guides for the eye.

3. Magnetic field dependence of acceptor-induced dielectric loss

We performed magnetic field dependence study with resonators on two types of boron-doped wafers. The results presented in Fig. 4 were measured on boron-doped wafer

no. 3 (float zone, $[B] = 7.4 \times 10^{14} \text{ cm}^{-3}$). Additional measurements were performed on resonators fabricated on boron-doped wafer no. 4 (Czochralski, $[B] = 2.5 \times 10^{15} \text{ cm}^{-3}$). The magnetic field dependence of Q_i is summarized in Fig. 8. The boron-induced dielectric loss is

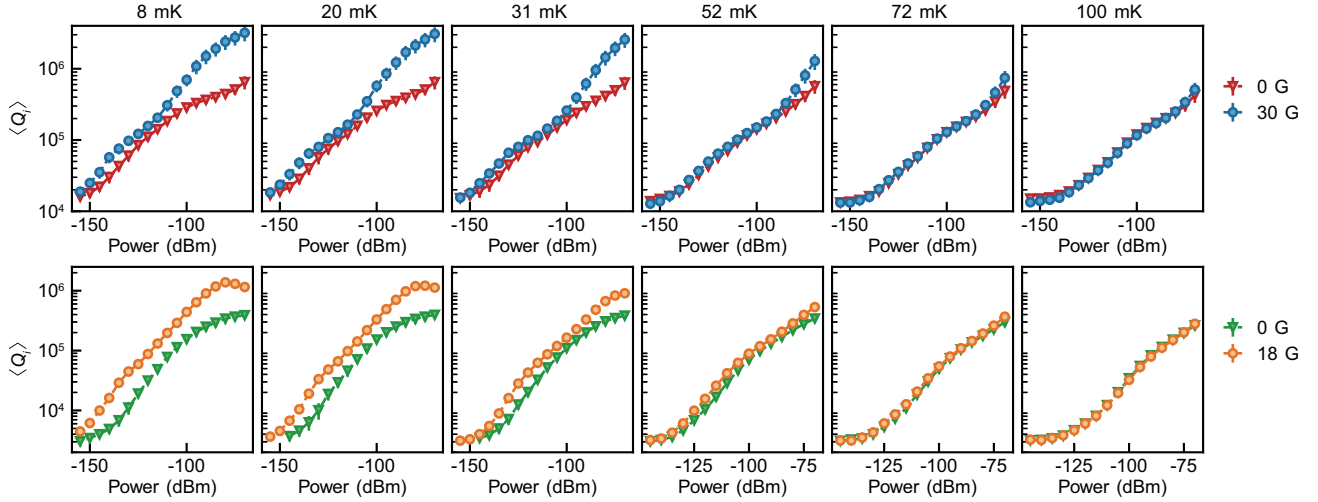


FIG. 9. Temperature dependence of the magnetic field response on resonators fabricated on a float-zone-grown substrate with $[B] = 7.4 \times 10^{14} \text{ cm}^{-3}$ (top row) and a Czochralski-grown substrate with $[B] = 2.5 \times 10^{15} \text{ cm}^{-3}$ (bottom row). The temperatures are specified at the mixing chamber plate.

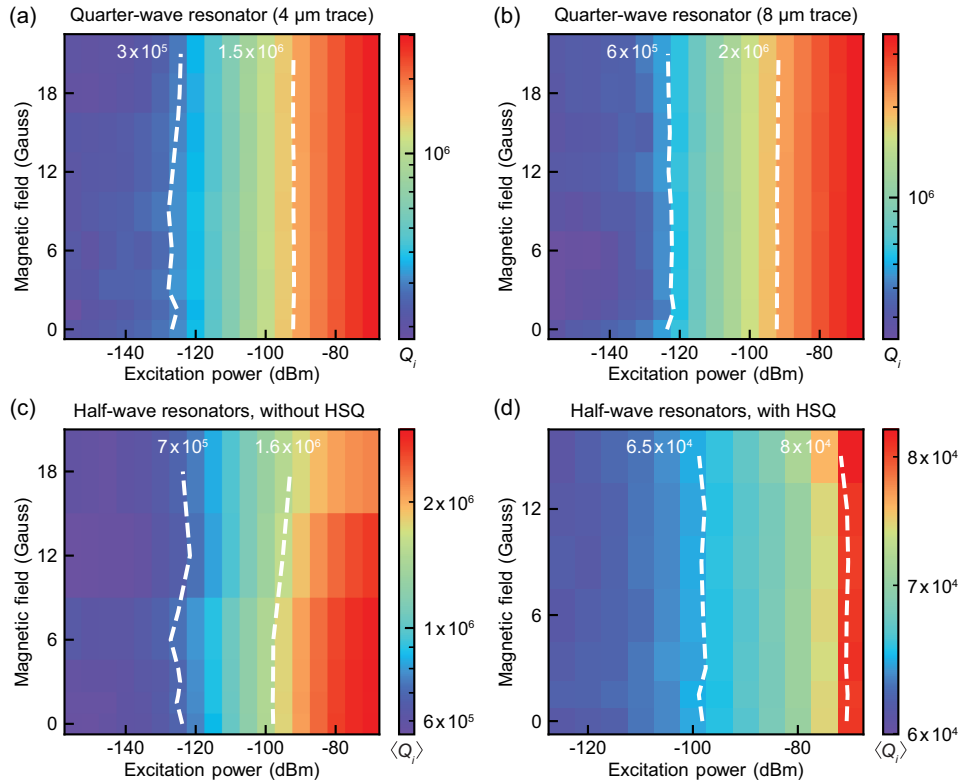


FIG. 10. Magnetic field dependence of Q_i on undoped substrates for quarter-wave resonators of different trace widths (a),(b) and half-wave resonators (c) before and (d) after HSQ coating. The dashed lines are interpolated contour lines as guides for the eye. No magnetic field response is observable in (a), (b), and (d). Q_i in (c) decreased slightly at higher fields due to vortex losses. Data in (c) and (d) represent the average Q_i of three resonators.

reduced upon applying a small magnetic field for both types of substrates.

The magnetic-field-induced loss reduction on boron-doped silicon shows a strong temperature dependence. At higher temperatures, the magnetic field response is suppressed. The temperature-dependent magnetic field response on resonators fabricated on two types of boron-doped substrates is summarized in Fig. 9.

4. Magnetic field dependence of amorphous TLS-induced dielectric loss

We performed extensive magnetic field dependence studies with conventional amorphous TLSs on resonators fabricated on undoped silicon. The results presented in Fig. 4(f) were measured on a quarter-wave resonator with a trace width of 2 μm . Additional measurements were performed on quarter-wave resonators with trace widths of 4 [Fig. 10(a)] and 8 μm [Fig. 10(b)]. Besides amorphous TLSs in native surface oxides, we also studied the magnetic field dependence of TLSs in HSQ, a type of spin-on-glass where amorphous TLS density is expected to be high, by drop casting HSQ on top of high- Q half-wave resonators fabricated on undoped silicon [Figs. 10(c) and 10(d)].

APPENDIX C: SUPPLEMENTARY ANALYSIS

1. Electronic structure of acceptors and donors

Donor and acceptor defects in silicon have been widely studied for quantum applications. Here, we compare the electronic structure of boron acceptors and phosphorus donors and discuss their impact on bulk dielectric loss in silicon.

The electronic structure of acceptor defects inherits the structure of the valence band maximum of silicon with a twofold orbital degeneracy and strong spin-orbit coupling [Fig. 11(a)] [38]. The acceptor-based spin-orbit system couples strongly to environmental perturbations from strain (H_S) and electric (H_E) fields. Therefore, the spin-orbit system based on acceptors can be described as an effective two-level system causing dielectric loss. In the context of spin qubits, these strong environmental sensitivities negatively influence the lifetime and coherence of acceptor spins [33]. Therefore, acceptor defects normally cannot constitute a good qubit system. The extreme sensitivity of acceptor defects to their local environment also results in a broad inhomogeneous distribution of the orbital splittings. This distribution can be particularly large in typical nano-fabricated devices due to additional lattice strain and electric fields.

On the other hand, the electronic structure of donor spins inherits the structure of conduction band minimum of silicon with a sixfold valley degeneracy [Fig. 11(b)]. With valley-orbit splitting, the $1s$ orbital is split into $1s(A)$, $1s(T)$, and $1s(E)$ orbitals. The lowest orbital,

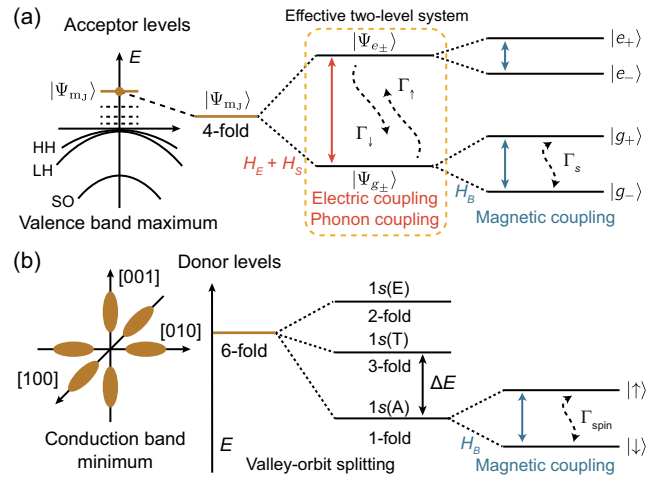


FIG. 11. Electronic structures of (a) acceptor and (b) donor defects. The nuclear spin degree of freedom is not shown for simplicity.

$1s(A)$, for phosphorus defects is 11.8 meV (approximately 3 THz, or an equivalent thermal energy of approximately 150 K) below the higher $1s(T)$ orbital [41]. Therefore, at cryogenic temperatures, phosphorus defects effectively provide an isolated spin degree of freedom in a singlet orbital. The lack of strong spin-orbit coupling makes phosphorus spins a good qubit system with long lifetimes and coherence times [31,32,34]. Regarding dielectric loss from phosphorus, no loss is expected from orbital transitions due to the large energy mismatch between the orbital splitting (approximately 3 THz) and microwave frequencies of interest for typical superconducting devices (<10 GHz). We note that donor-induced loss can occur at the spin resonance frequency due to magnetic coupling between donor spins and microwave resonators. However, such effects are significant at a large magnetic field for phosphorus ($g = 2$) spins (approximately 2000 G for a 5.6 GHz spin resonance). Additionally, such donor spin-induced loss will be a narrow-band effect due to the narrow inhomogeneous distribution of the spin resonance frequencies.

2. Strain at the metal-silicon interface

In our experiment, we observe a broadband (>1 GHz) boron-induced dielectric loss in all samples. This indicates that the orbital transition frequency of boron acceptors has a large inhomogeneous distribution, even though no intentional strain or electric field biases were applied. Such a large inhomogeneous distribution can originate from strain at the metal-silicon interface due to differential thermal contraction of the thin metal film and silicon substrate upon cooling the sample from the film deposition temperature to cryogenic temperatures [39].

At room temperature, we characterize the niobium film stress to be a compressive stress of 150 MPa on a

prime-grade silicon wafer. Using the film stress at room temperature as the initial condition, we perform finite-element simulation of strain induced by differential thermal contraction using COMSOL MULTIPHYSICS. For niobium, we used a Young's modulus of 105 GPa, a Poisson ratio of 0.4, and a temperature-dependent coefficient of thermal expansion [67]. For silicon, we used an anisotropic model for its elasticity matrix ($D_{11} = 166$ GPa, $D_{12} = 64$ GPa, and $D_{44} = 80$ GPa) and a temperature-dependent coefficient of thermal expansion [68].

In Fig. 12, we show the simulated strain distribution for the low-surface participation ratio resonator (trace width of 50 μm , gap width of 33.75 μm) at 10 mK. Near the edges of the metal film, the strain can be as high as 2×10^{-5} and can extend deep into the bulk. Therefore, this thermal strain is a possible origin of the broad inhomogeneous distribution of boron orbital splittings. We note that our simulation uses linear elastic approximation for thin-film niobium and does not consider its yield behavior (transition from elastic behavior to plastic behavior). Therefore, the simulated thermal strain provides only a simple, order-of-magnitude estimation for a rather complicated strain environment.

3. First-principles estimation of acceptor-induced dielectric loss

Before providing a first-principles estimation of acceptor-induced loss, we first qualitatively estimate the loss from amorphous TLSs and from boron defects based on their effective density and the respective energy participation ratio for our low surface participation ratio resonator. For TLSs, we assume a density of $10^{14} \text{ cm}^{-3} \text{ GHz}^{-1}$ [69]. For boron-doped silicon, the effective density of boron defects depends on the inhomogeneous distribution of boron resonances, which strongly depends on static stray strain and electric field in the silicon substrate. For a doping

concentration of $1.0 \times 10^{15} \text{ cm}^{-3}$ (15 $\Omega \text{ cm}$) and a conservative inhomogeneous distribution of 100 GHz, the effective density is $10^{13} \text{ cm}^{-3} \text{ GHz}^{-1}$. The energy participation ratio for surface TLSs in the low surface participation ratio design is 4.5×10^{-4} , while the energy participation ratio for boron in bulk defects silicon is $\epsilon_r/(1 + \epsilon_r) \approx 0.92$, where ϵ_r is the dielectric constant of silicon. With these parameters and assuming similar electric dipole moments for TLSs and boron defects, the acceptor-induced loss will be 200 times more compared to TLS-induced loss.

From the above discussion, we see that acceptor-induced loss can far exceed TLS-induced loss at high doping concentrations. The loss estimation depends strongly on the inhomogeneous distribution of boron resonances. We calculate the spatial distribution of boron orbital splittings for the low surface participation ratio resonator using the thermal strain and boron Hamiltonian [Eqs. (2)–(4) in the main text and Fig. 13(a)]. The spatial distribution shows that the orbital splitting can be as high as 100 GHz near the surface, and strain-induced splittings in the boron ensemble can extend deep in the bulk. The energy participation in the bulk is also spatially dependent [Fig. 13(b)]. Therefore, it is critical to include spatial dependences of both energy participation and boron resonances to estimate the boron-induced dielectric loss.

Defect-induced dielectric loss can be estimated from the first principles using the imaginary part of atomic susceptibility: $\chi''(f, f_0) = \mu^2 N g(f, f_0) / (2\epsilon_0 \hbar)$, where μ is the electric transition dipole moment, ϵ_0 is the vacuum permittivity, N represents the volumetric dopant density, and $g(f, f_0)$ represents the normalized Lorentzian line shape of the atomic transition with a resonance frequency f_0 [70].

For a generic device geometry, the observed loss tangent at frequency f is a participation-ratio averaged loss tangent:

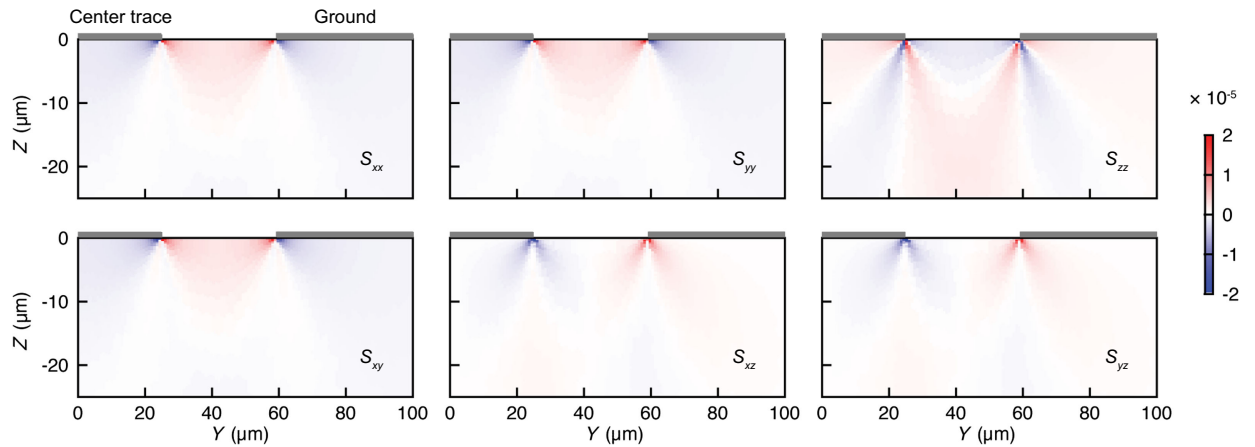


FIG. 12. Strain distribution at the metal-silicon interface from differential thermal contraction. Half of the cross section is shown due to the symmetry of the geometry. The strain tensor components are given in the cubic [100] basis (xyz). The Z direction is aligned with the silicon [001] direction, while the Y direction is aligned with the silicon [110] direction, based on the silicon wafer orientation and the sample cut directions.

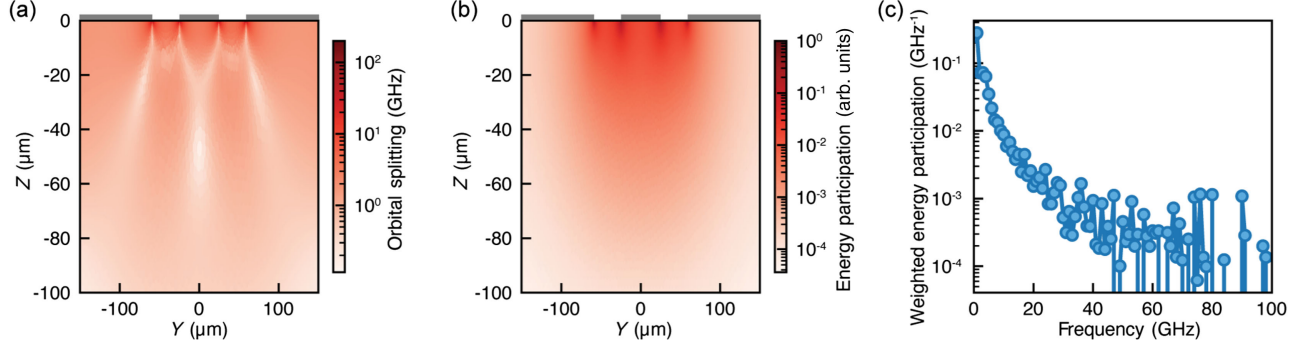


FIG. 13. (a) Spatial distribution of boron orbital splittings due to thermal strain at the metal-silicon interface. (b) Spatial distribution of electrical energy in silicon. (c) Weighted energy participation $[P(f_0)]$ of boron acceptors as a function of boron orbital splittings.

$$\overline{\tan \delta_0}(f) = \int_V p(r) \tan \delta_0(f, r) dV, \quad (\text{C1})$$

where $p(r)$ represents the volumetric density of bulk energy participation ratio $[\int_V p(r) dV \approx 0.92]$ and $\tan \delta_0(f, r)$ denotes a spatially varying loss tangent as a function of spatial location r .

The spatial dependence in loss tangent arises from the spectral inhomogeneity of boron resonances due to the spatially varying strain. The defect-induced loss tangent can be calculated from the imaginary part of atomic susceptibility:

$$\tan \delta_0(f, r) = \int_{f_0} \frac{q(f_0, r) \chi''(f, f_0)}{\epsilon_r} df_0, \quad (\text{C2})$$

where $q(f_0, r)$ denotes the spectral distribution of boron resonances at location r $[\int q(f_0, r) df_0 = 1]$ and ϵ_r represents the dielectric constant of silicon. Combining Eqs. (C1) and (C2), the observed loss tangent is represented by a double integral over space and frequency:

$$\overline{\tan \delta_0}(f) = \int_V \int_{f_0} \frac{p(r) q(f_0, r) \chi''(f, f_0)}{\epsilon_r} df_0 dV. \quad (\text{C3})$$

We can evaluate the volume integral of $p(r)q(f_0, r)$ numerically using a uniform sampling of the spatial distribution of boron orbital splittings [Fig. 13(a)] and energy participation [Fig. 13(b)]:

$$\begin{aligned} P(f_0) &= \int_V p(r) q(f_0, r) dV \\ &= \sum_V p(r) \Delta V \times q(f_0, r), \end{aligned} \quad (\text{C4})$$

where $p(r)\Delta V$ represents the energy participation ratio in volume ΔV . For each small volume ΔV , we assume all the boron acceptors inside share the same orbital splitting. Therefore, we can numerically evaluate the weighted energy participation $P(f_0)$ in the unit of GHz^{-1} as a

function of frequency f_0 [Fig. 13(c)]. Near our device frequencies (approximately 6 GHz), $P(f_0 = 6 \text{ GHz}) \approx 0.03/\text{GHz}$. Physically, $P(f_0 = 6 \text{ GHz}) \approx 0.03/\text{GHz}$ means 3% of the total electrical energy is experiencing dielectric loss from boron defects distributed in a 1 GHz band around 6 GHz.

In the low-power limit free from atomic saturation effects, the dielectric loss tangent is

$$\overline{\tan \delta_0}(f) = \int \chi''(f, f_0) P(f_0) df_0 / \epsilon_r. \quad (\text{C5})$$

With a smooth, slowly varying $P(f_0)$, we have

$$\begin{aligned} \overline{\tan \delta_0}(f) &= \int \chi''(f, f_0) P(f_0) df_0 / \epsilon_r \\ &= P(f) \int \chi''(f, f_0) df_0 / \epsilon_r \\ &= \frac{\mu^2 P(f)}{2\epsilon_0 \epsilon_r \hbar} N. \end{aligned} \quad (\text{C6})$$

For our silicon wafer with the highest boron concentration ($N = 2.5 \times 10^{15} \text{ cm}^{-3}$), using $P(\nu = 6 \text{ GHz}) = 0.03/\text{GHz}$ and $\mu = \sqrt{1/3} \times 0.26 \text{ D}$, we estimate the boron-limited quality factor $[1/\overline{\tan \delta_0}(f = 6 \text{ GHz})]$ to be approximately 1×10^6 . The factor of $\sqrt{1/3}$ in μ accounts for the random alignment of the electric dipole moment with respect to the direction of the electric field from the resonator. Interestingly, this first-principles estimation of quality factor is about 400 times higher than our experimental observation. Further investigation is needed to resolve the discrepancy. The difference may be accounted by a combination of (i) a different inhomogeneous distribution from unaccounted strain contributions beyond the simplified thermal strain, (ii) the modification of electric dipole moment with the static stray strain [61], and (iii) the electric dipole moment being much higher than the literature values in Ref. [36]. We note that the electric dipole moment was estimated from dielectric loss measurement on unstrained

silicon in Ref. [36]. In future work, it would be interesting to perform a Stark shift measurement on single boron acceptors to extract the electric field coupling coefficients more accurately.

4. Geometry dependence of acceptor-induced dielectric loss

As discussed in the main text and in Appendix C 3, the acceptor-induced dielectric loss is expected to be strongly strain dependent. In our samples, there will be a spatially dependent interface strain due to differential thermal contraction of metal and silicon. With different resonator geometries, boron acceptors in different strain environment will be probed. Therefore, the apparent dielectric loss in boron-doped silicon may be resonator geometry dependent.

In the surface participation sweep study [Fig. 2(b)], we observed bulk-limited loss in boron-doped silicon. There appears to be a weak positive correlation between surface participation and the bulk-limited Q_i . We emphasize that the magnitude of such trend is small compared to the scatter of data. However, such a trend, if any, may be explained by geometry-dependent loss. For example, resonators with larger surface participation will probe dielectric loss originating from shallower boron defects which may experience higher strain and overall exhibit orbital splittings that are detuned to higher frequencies than the resonator frequency.

We simulated the inhomogeneous distribution of boron defects for a high surface participation ratio resonator with a trace width of 2 μm [Fig. 14(a)]. The electric volume of the resonator [Fig. 14(b)] is much smaller than that of the resonator with a 50 μm trace width [Fig. 13(b)]. Therefore, the resonator is more sensitive to shallow boron defects. We numerically evaluate the weighted energy participation for this resonator design as shown in Fig. 14(c). The weighted energy participation for the high surface participation ratio resonator shows a different frequency dependence compared to the low surface participation ratio resonator [Fig. 13(c)]. Therefore, the bulk loss tangent will appear different when measured with these different resonator geometries.

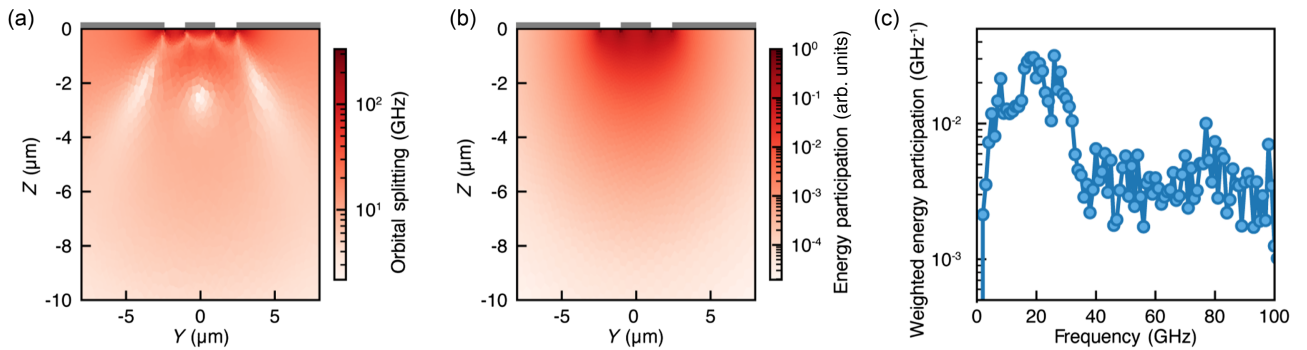


FIG. 14. (a) Spatial distribution of boron orbital splittings due to thermal strain at the metal-silicon interface. (b) Spatial distribution of electrical energy in silicon. (c) Weighted energy participation [$P(f_0)$] of boron acceptors as a function of boron orbital splittings. The simulated resonator geometry has a trace width of 2 μm and a gap width of 1.42 μm .

5. Theoretical analysis of saturation behavior for a four-level system

Defect-induced dielectric loss can be saturated with microwave excitation and/or thermal excitation. The saturation behavior depends strongly on the detailed electronic structure of the defect. For the case of boron acceptors, the electronic structure under static crystal strain is a four-level system with a twofold degeneracy in the two orbital branches [Fig. 15(a)]. Under a small magnetic field, the level degeneracy is lifted, and the electronic structure contains four distinct levels with generalized spin sublevels [Fig. 15(b)]. In this case, the generalized spin states can have long lifetimes [33]. We observe that applying a small magnetic field can lead to strong reduction of boron-induced loss (Figs. 4 and 8). At the same time, the magnetic response disappears at elevated temperatures (Fig. 9). In this section, we perform theoretical analysis of saturation power of a four-level system under different conditions.

The electric and strain couplings of boron levels depend strongly on the details of static crystal strain. To reduce the complexity of the problem, our analysis is performed assuming static tensile strain with a single tone drive. Under tensile strain, only $|1\rangle \leftrightarrow |3\rangle$ and $|2\rangle \leftrightarrow |4\rangle$ transitions are electric dipole allowed. At the same time, $|1\rangle \leftrightarrow |3\rangle$ and $|2\rangle \leftrightarrow |4\rangle$ ($|1\rangle \leftrightarrow |4\rangle$ and $|2\rangle \leftrightarrow |3\rangle$) transitions share the same spontaneous phonon emission rate γ' ($\tilde{\gamma}$).

Four-level system at zero magnetic field.—The saturation behavior of defect-induced dielectric loss can be related to the population difference of the ground and excited states in steady state [70]. The Hamiltonian of a four-level system [Fig. 15(a)] in the rotating frame of a resonant drive is

$$H/\hbar = \Omega^*(|1\rangle\langle 3| + |2\rangle\langle 4|) + \Omega(|3\rangle\langle 1| + |4\rangle\langle 2|). \quad (\text{C7})$$

The system evolves following the Lindblad master equation:

$$\dot{\rho} = -\frac{i}{\hbar}[H, \rho] + \sum_i \mathcal{D}[C_i]\rho \quad (\text{C8})$$

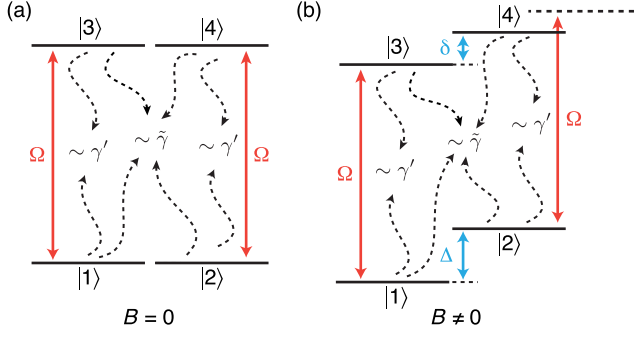


FIG. 15. Level diagram with a resonant single-tone drive for a four-level system (a) at zero magnetic field and (b) at a nonzero magnetic field. Ω denotes the driving strength. δ and Δ denote the Zeeman splittings within the two orbital branches. γ' and $\tilde{\gamma}$ denote the relevant spontaneous decay rates. The actual orbital decay rates also include thermally assisted processes.

with the superoperator defined as $\mathcal{D}[C]\rho = C\rho C^\dagger - \frac{1}{2}(C^\dagger C\rho + \rho C^\dagger C)$. There are eight collapse operators denoting the phonon-assisted relaxation paths: $C_1 = \sqrt{\bar{n}\gamma'}|3\rangle\langle 1|$, $C_2 = \sqrt{(\bar{n}+1)\gamma'}|1\rangle\langle 3|$, $C_3 = \sqrt{\bar{n}\tilde{\gamma}}|3\rangle\langle 2|$, $C_4 = \sqrt{(\bar{n}+1)\tilde{\gamma}}|2\rangle\langle 3|$, $C_5 = \sqrt{\bar{n}\tilde{\gamma}}|4\rangle\langle 1|$, $C_6 = \sqrt{(\bar{n}+1)\tilde{\gamma}} \times |1\rangle\langle 4|$, $C_7 = \sqrt{\bar{n}\gamma'}|4\rangle\langle 2|$, and $C_8 = \sqrt{(\bar{n}+1)\gamma'}|2\rangle\langle 4|$. \bar{n} denotes the thermal phonon occupancy, and γ' and $\tilde{\gamma}$ are the spontaneous phonon emission rates from $|3\rangle \rightarrow |1\rangle$ ($|4\rangle \rightarrow |2\rangle$) and $|3\rangle \rightarrow |2\rangle$ ($|4\rangle \rightarrow |1\rangle$), respectively. Based on the master equation, the equations of motion describing the evolution of population and coherences can be written as

$$\dot{\rho}_{11} = -(\gamma' + \tilde{\gamma})\bar{n}\rho_{11} + (1 + \bar{n})(\gamma'\rho_{33} + \tilde{\gamma}\rho_{44}) + i\Omega\rho_{13} - i\Omega^*\rho_{31}, \quad (\text{C9})$$

$$\dot{\rho}_{22} = -(\gamma' + \tilde{\gamma})\bar{n}\rho_{22} + (1 + \bar{n})(\tilde{\gamma}\rho_{33} + \gamma'\rho_{44}) + i\Omega\rho_{24} - i\Omega^*\rho_{42}, \quad (\text{C10})$$

$$\dot{\rho}_{33} = -(\gamma' + \tilde{\gamma})(1 + \bar{n})\rho_{33} + \bar{n}(\tilde{\gamma}\rho_{22} + \gamma'\rho_{11}) + i\Omega^*\rho_{31} - i\Omega\rho_{13}, \quad (\text{C11})$$

$$\dot{\rho}_{13} = -(\gamma' + \tilde{\gamma})(1/2 + \bar{n})\rho_{13} + i\Omega^*(\rho_{11} - \rho_{33}), \quad (\text{C12})$$

$$\dot{\rho}_{24} = -(\gamma' + \tilde{\gamma})(1/2 + \bar{n})\rho_{24} + i\Omega^*(\rho_{22} - \rho_{44}), \quad (\text{C13})$$

$$\dot{\rho}_{12} = -(\gamma' + \tilde{\gamma})\bar{n}\rho_{12} + i(\Omega\rho_{14} - \Omega^*\rho_{32}), \quad (\text{C14})$$

$$\dot{\rho}_{14} = -(\gamma' + \tilde{\gamma})(1/2 + \bar{n})\rho_{14} + i\Omega^*(\rho_{12} - \rho_{34}), \quad (\text{C15})$$

$$\dot{\rho}_{23} = -(\gamma' + \tilde{\gamma})(1/2 + \bar{n})\rho_{23} + i\Omega^*(\rho_{21} - \rho_{43}), \quad (\text{C16})$$

$$\dot{\rho}_{34} = -(\gamma' + \tilde{\gamma})(1 + \bar{n})\rho_{34} + i\Omega^*\rho_{32} - i\Omega\rho_{14}. \quad (\text{C17})$$

We note that $\rho_{ij} = \rho_{ji}^*$ and $\rho_{11} + \rho_{22} + \rho_{33} + \rho_{44} = 1$. Population in the steady state ($\dot{\rho}_{ij} = 0$ and $\dot{\rho}_{ii} = 0$) can be solved as

$$\rho_{11} = \rho_{22} = \frac{1}{2} \times \frac{(1 + \bar{n})(\gamma' + \tilde{\gamma}) + R}{(1 + 2\bar{n})(\gamma' + \tilde{\gamma}) + 2R}, \quad (\text{C18})$$

$$\rho_{33} = \rho_{44} = \frac{1}{2} \times \frac{\bar{n}(\gamma' + \tilde{\gamma}) + R}{(1 + 2\bar{n})(\gamma' + \tilde{\gamma}) + 2R}, \quad (\text{C19})$$

where $R = 4|\Omega|^2/[(1 + 2\bar{n})(\gamma' + \tilde{\gamma})]$ is a pumping rate. Note that if $R \gg (\gamma' + \tilde{\gamma})(\bar{n} + \frac{1}{2})$, we achieve equal population in the ground and excited states ($\rho_{11} = \rho_{22} = \rho_{33} = \rho_{44} = 1/4$).

In order to quantify the critical Rabi frequency, we define the saturation condition as $\rho_{11} - \rho_{33} = (\rho_{11} - \rho_{33})_0/\sqrt{2}$, where $(\rho_{11} - \rho_{33})_0 = 1/(4\bar{n} + 2)$ is the initial population difference at thermal equilibrium under no drive. The critical Rabi frequency that achieves this condition is

$$|\Omega_c(B=0)|^2 = \frac{(\gamma' + \tilde{\gamma})^2}{8} (2\bar{n} + 1)^2 (\sqrt{2} - 1). \quad (\text{C20})$$

We note that Eq. (C20) also holds for a pure two-level system with a spontaneous decay rate of $\gamma' + \tilde{\gamma}$. This validates the two-level system approximation when no magnetic field is applied.

Four-level system in a magnetic field.—Under a magnetic field, the electronic structure of boron is a four-level system with different Zeeman splittings (Δ and δ) in the two orbital branches. The Hamiltonian of such four-level system [Fig. 15(b)] in the rotating frame of the drive can be written as

$$H/\hbar = \Delta|2\rangle\langle 2| + \delta|4\rangle\langle 4| + \Omega(|3\rangle\langle 1| + |4\rangle\langle 2|) + \Omega^*(|1\rangle\langle 3| + |2\rangle\langle 4|). \quad (\text{C21})$$

Similar to the zero magnetic field case, there are eight collapse operators denoting the phonon-assisted decay paths: $C_1 = \sqrt{\bar{n}\gamma'}|3\rangle\langle 1|$, $C_2 = \sqrt{(\bar{n}+1)\gamma'}|1\rangle\langle 3|$, $C_3 = \sqrt{\bar{n}\tilde{\gamma}}|3\rangle\langle 2|$, $C_4 = \sqrt{(\bar{n}+1)\tilde{\gamma}}|2\rangle\langle 3|$, $C_5 = \sqrt{\bar{n}\tilde{\gamma}}|4\rangle\langle 1|$, $C_6 = \sqrt{(\bar{n}+1)\tilde{\gamma}} \times |1\rangle\langle 4|$, $C_7 = \sqrt{\bar{n}\gamma'}|4\rangle\langle 2|$, and $C_8 = \sqrt{(\bar{n}+1)\gamma'}|2\rangle\langle 4|$. \bar{n} denotes the thermal phonon occupancy, and γ' and $\tilde{\gamma}$ are the spontaneous emission rates from $|3\rangle \rightarrow |1\rangle$ ($|4\rangle \rightarrow |2\rangle$) and $|3\rangle \rightarrow |2\rangle$ ($|4\rangle \rightarrow |1\rangle$), respectively. The spin lifetime within each orbital branch is much longer than orbital lifetimes [33]. Therefore, we neglect the spin relaxation process between $|2\rangle \leftrightarrow |1\rangle$.

Assuming radiative decoherence only, we obtain the equations of motion for the populations and coherences using the Lindblad master equation [Eq. (C8)]:

$$\begin{aligned} \dot{\rho}_{11} = & -(\gamma' + \tilde{\gamma})\bar{n}\rho_{11} + (1 + \bar{n})(\gamma'\rho_{33} + \tilde{\gamma}\rho_{44}) \\ & + i\Omega\rho_{13} - i\Omega^*\rho_{31}, \end{aligned} \quad (\text{C22})$$

$$\begin{aligned} \dot{\rho}_{22} = & -(\gamma' + \tilde{\gamma})\bar{n}\rho_{22} + (1 + \bar{n})(\tilde{\gamma}\rho_{33} + \gamma'\rho_{44}) \\ & + i\Omega\rho_{24} - i\Omega^*\rho_{42}, \end{aligned} \quad (\text{C23})$$

$$\begin{aligned} \dot{\rho}_{33} = & -(\gamma' + \tilde{\gamma})(1 + \bar{n})\rho_{33} + \bar{n}(\tilde{\gamma}\rho_{22} + \gamma'\rho_{11}) \\ & - i\Omega\rho_{13} + i\Omega^*\rho_{31}, \end{aligned} \quad (\text{C24})$$

$$\dot{\rho}_{13} = -(\gamma' + \tilde{\gamma})(1/2 + \bar{n})\rho_{13} + i\Omega^*(\rho_{11} - \rho_{33}), \quad (\text{C25})$$

$$\begin{aligned} \dot{\rho}_{24} = & -(\gamma' + \tilde{\gamma})(1/2 + \bar{n})\rho_{24} + i(\delta - \Delta)\rho_{24} \\ & + i\Omega^*(\rho_{22} - \rho_{44}), \end{aligned} \quad (\text{C26})$$

$$\dot{\rho}_{12} = -(\gamma' + \tilde{\gamma})\bar{n}\rho_{12} + i\Delta\rho_{12} + i\Omega\rho_{14} - i\Omega^*\rho_{32}, \quad (\text{C27})$$

$$\begin{aligned} \dot{\rho}_{14} = & -(\gamma' + \tilde{\gamma})(1/2 + \bar{n})\rho_{14} + i\delta\rho_{14} \\ & + i\Omega^*(\rho_{12} - \rho_{34}), \end{aligned} \quad (\text{C28})$$

$$\begin{aligned} \dot{\rho}_{23} = & -(\gamma' + \tilde{\gamma})(1/2 + \bar{n})\rho_{23} - i\Delta\rho_{23} \\ & + i\Omega^*(\rho_{21} - \rho_{43}), \end{aligned} \quad (\text{C29})$$

$$\begin{aligned} \dot{\rho}_{34} = & -(\gamma' + \tilde{\gamma})(1 + \bar{n})\rho_{34} + i\delta\rho_{34} + i\Omega^*\rho_{32} \\ & - i\Omega\rho_{14}. \end{aligned} \quad (\text{C30})$$

For large detuning ($|\Delta - \delta| \gg |\Omega|$), we can ignore the coherences between transitions detuned from the drive ($\rho_{24} \approx 0$, $\rho_{23} \approx 0$, $\rho_{14} \approx 0$, $\rho_{12} \approx 0$). The steady state populations and coherences under drive can then be evaluated with $\dot{\rho}_{11} = \dot{\rho}_{22} = \dot{\rho}_{33} = \dot{\rho}_{13} = 0$ (steady state condition) and $\rho_{11} + \rho_{22} + \rho_{33} + \rho_{44} = 1$ (conservation of population):

$$\rho_{11} = \frac{\bar{n}(1 + \bar{n})[2(1 + \bar{n})\gamma'(\gamma' + \tilde{\gamma}) + R(2\gamma' + \tilde{\gamma})]}{R[1 + 8\bar{n}(1 + \bar{n})]\gamma' + R(1 + 2\bar{n})^2\tilde{\gamma} + 4\bar{n}(1 + \bar{n})(1 + 2\bar{n})\gamma'(\gamma' + \tilde{\gamma})}, \quad (\text{C31})$$

$$\rho_{22} = \frac{(1 + \bar{n})[2\bar{n}(1 + \bar{n})\gamma'(\gamma' + \tilde{\gamma}) + R(\gamma' + 2\bar{n}\gamma' + \tilde{\gamma} + \bar{n}\tilde{\gamma})]}{R[1 + 8\bar{n}(1 + \bar{n})]\gamma' + R(1 + 2\bar{n})^2\tilde{\gamma} + 4\bar{n}(1 + \bar{n})(1 + 2\bar{n})\gamma'(\gamma' + \tilde{\gamma})}, \quad (\text{C32})$$

$$\rho_{33} = \frac{\bar{n}(1 + \bar{n})[2\bar{n}\gamma'(\gamma' + \tilde{\gamma}) + R(2\gamma' + \tilde{\gamma})]}{R[1 + 8\bar{n}(1 + \bar{n})]\gamma' + R(1 + 2\bar{n})^2\tilde{\gamma} + 4\bar{n}(1 + \bar{n})(1 + 2\bar{n})\gamma'(\gamma' + \tilde{\gamma})}, \quad (\text{C33})$$

$$\rho_{44} = \frac{\bar{n}[2\bar{n}(1 + \bar{n})\gamma'(\gamma' + \tilde{\gamma}) + R(\gamma' + 2\bar{n}\gamma' + \bar{n}\tilde{\gamma})]}{R[1 + 8\bar{n}(1 + \bar{n})]\gamma' + R(1 + 2\bar{n})^2\tilde{\gamma} + 4\bar{n}(1 + \bar{n})(1 + 2\bar{n})\gamma'(\gamma' + \tilde{\gamma})}, \quad (\text{C34})$$

where $R = 4|\Omega|^2/[(1 + 2\bar{n})(\gamma' + \tilde{\gamma})]$ is a pumping rate. We observe that $\rho_{22} > \rho_{11}$ holds with $R > 0$. This shows the generation of ground state population imbalance with a selective drive. The optical pumping process is competing with the phonon-assisted relaxation process that depletes ρ_{22} at a rate of $\bar{n}(\gamma' + \tilde{\gamma})$. When $R \gg \bar{n}(\gamma' + \tilde{\gamma})$ and $\bar{n} \ll 1$, the ground state is fully polarized ($\rho_{22} \approx 1$).

In order to quantitatively calculate the critical Rabi frequency, we define the saturation condition as $\rho_{11} - \rho_{33} = (\rho_{11} - \rho_{33})_0/\sqrt{2}$, where $(\rho_{11} - \rho_{33})_0 = 1/(4\bar{n} + 2)$ is the initial population difference at thermal equilibrium under no drive. The critical Rabi frequency that achieves this condition is

$$|\Omega_c(B > 0)|^2 = \frac{\bar{n}(1 + \bar{n})(1 + 2\bar{n})^2\gamma'(\gamma' + \tilde{\gamma})^2(\sqrt{2} - 1)}{\gamma' + 8\bar{n}(1 + \bar{n})\gamma' + \tilde{\gamma} + 4\bar{n}(1 + \bar{n})\tilde{\gamma}}. \quad (\text{C35})$$

Comparing Eqs. (C20) and (C35), we can calculate the ratio of saturation power for a four-level system with and without magnetic field:

$$\begin{aligned} \frac{P_c(B = 0)}{P_c(B > 0)} &= \frac{n_c(B = 0)}{n_c(B > 0)} \\ &= \left| \frac{\Omega_c(B = 0)}{\Omega_c(B > 0)} \right|^2 \\ &= 1 + \frac{1}{8\bar{n}(\bar{n} + 1)} + \frac{\tilde{\gamma}}{8\bar{n}(\bar{n} + 1)\gamma'} + \frac{\tilde{\gamma}}{2\gamma'}. \end{aligned} \quad (\text{C36})$$

Two remarks can be made here. (i) The ratio of saturation power with and without a magnetic field is greater than 1. This is consistent with the intuition that the ability to pump into a dark state reduces saturation power. (ii) The magnetic-field-induced contrast has a $1/\bar{n}$ dependence for $n \ll 1$ and is, therefore, strongly temperature dependent. We fit the temperature dependence of the saturation power change induced by a magnetic field on two samples with high boron doping. The generic form of power-dependent loss tangent for superconducting resonators is expressed as

$$\tan \delta = \tan \delta_0 \frac{A(T)}{\sqrt{1 + (\frac{n}{n_c})^\beta}}, \quad (\text{C37})$$

where $\tan \delta_0$ indicates the loss tangent with no drive at zero temperature, n_c denotes the critical photon number that suppresses the loss by $\sqrt{2}$, β is a geometry-dependent fit parameter, and $A(T) = \tanh[\hbar\omega/(2k_B T)]$ represents thermal saturation. The fitting parameter β , which is not captured in theory, is phenomenologically added to account for electrical field distribution. We perform our analysis in a regime where $n/n_c \gg 1$, such that

$$\begin{aligned} \log(\tan \delta) &= \log(A(T) \tan \delta_0) - \frac{1}{2} \log \left[1 + \left(\frac{n}{n_c} \right)^\beta \right] \\ &\approx \log(A(T) \tan \delta_0) - \frac{\beta}{2} \log(n) + \frac{\beta}{2} \log(n_c). \end{aligned} \quad (\text{C38})$$

We fit the data in Fig. 9 to $\log(\tan \delta) = -a \log(n) + b$, where $a = \beta/2$ and $b = \log(A(T) \tan \delta_0) + (\beta/2) \log(n_c)$ are fit parameters, as seen in Figs. 16(a) and 16(b). The fit parameter a (resonator geometry dependent) is shared at a given temperature for both $B = 0$ and $B > 0$ cases. Note that $\Delta b = b(B = 0) - b(B > 0) = a \log(n_c(B = 0)/n_c(B > 0))$ when we assume the zero-power loss tangent is magnetic field independent [$A(T) \tan \delta_0(B = 0) = A(T) \tan \delta_0(B > 0)$]. Therefore, the ratio between critical photon numbers can be calculated as

$$\frac{n_c(B = 0)}{n_c(B > 0)} = 10^{\Delta b/a}. \quad (\text{C39})$$

In Fig. 16(c), we plot the experimentally extracted ratios of critical photon numbers as a function of temperature for two boron-doped samples and compare them to the theoretical prediction based on Eq. (C36). For both samples, we observe that the critical photon number is reduced by approximately an order of magnitude with an applied magnetic field at our base temperature (8 mK). At the same time, the magnetic field response disappears at slightly elevated temperatures around 100 mK. The experimental results qualitatively share the similar temperature-dependent behavior as the theoretical prediction. However, the experimental temperature is about 65 mK lower than the theoretical prediction to achieve the same ratio of critical photon numbers. This discrepancy can be accounted for if the actual sample temperature is higher than the temperature reading of the mixing chamber of the fridge. Indeed, we observed a non-negligible thermal excited state population (2.8%) for a superconducting transmon qubit at 6.3 GHz measured in the same setup [56]. This excited state population translates to a chip temperature of 84 mK when the mixing chamber temperature reads 10 mK. The inferred effective temperature here is comparable to the effective temperatures reported in other studies [43–46]. Therefore,

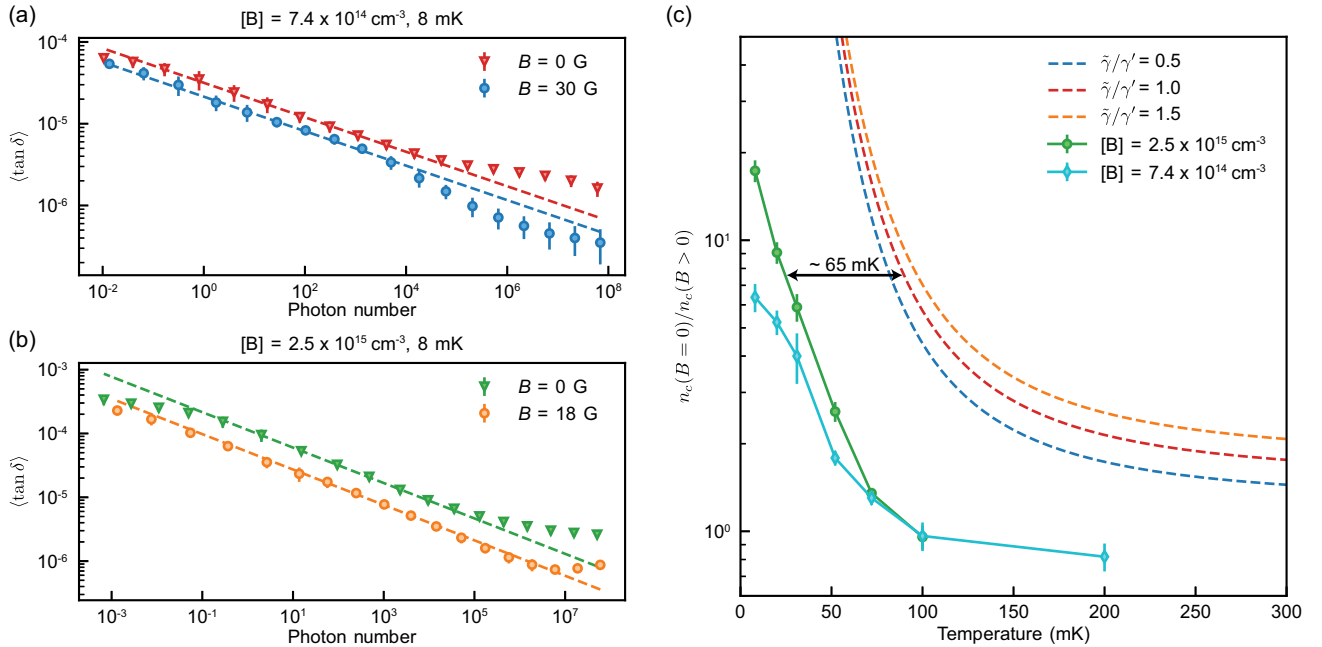


FIG. 16. Power dependence of average loss tangent of eight resonators at $T_{\text{MXC}} = 8$ mK with and without magnetic field in (a) a float-zone-grown substrate with $[B] = 7.4 \times 10^{14} \text{ cm}^{-3}$ and (b) a Czochralski-grown substrate with $[B] = 2.5 \times 10^{15} \text{ cm}^{-3}$. The dashed lines are linear fits between $\log(\tan \delta)$ and $\log(n)$ based on Eq. (C38). (c) Theoretical and experimental critical photon number ratio with and without magnetic field as a function of temperature for two boron doping concentrations and three branching ratios ($\tilde{\gamma}/\gamma'$). In theoretical calculations, we use the average frequency (approximately 6.1 GHz) of our resonators to convert thermal occupancy to temperature.

we expect a higher contrast in magnetic field response when the sample is better thermalized.

Even though Eq. (C36) explains the qualitative trend of the saturation photon number ratio, it does not capture all the experimental observations. We note that the high-temperature critical photon number ratio is estimated higher in theory. The discrepancy between our experiment and the theory may originate from (i) our master equation model takes into account only the boron defects on resonance with the resonator—the large bath of off-resonant boron defects can also lead to loss and are not accounted—and (ii) the fitting parameter β is not predicted by theory but rather a phenomenologically included parameter to account for electric field distribution in a real device.

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